



Archived by Flinders University

This is the peer reviewed version of the following article:

Jazayeri, A., & Werner, A. D. (2019). Boundary Condition Nomenclature Confusion in Groundwater Flow Modeling. *Groundwater*, 57(5), 664–668

which has been published in final form at

<https://doi.org/10.1111/gwat.12893>

This article may be used for non-commercial purposes in accordance with Wiley Terms and Conditions for self-archiving.

Copyright © 2019 John Wiley & Sons, Inc.
All rights reserved.

Technical Commentary

Boundary condition nomenclature confusion in groundwater flow modelling

Amir Jazayeri^{1,2}, Adrian D. Werner^{1,2*}

¹National Centre for Groundwater Research and Training, Flinders University, GPO Box 2100, Adelaide, SA 5001, Australia.

²College of Science and Engineering, Flinders University, GPO Box 2100, Adelaide, SA 5001, Australia.

*Corresponding author

Email addresses:

Amir Jazayeri: amir.jazayeri@flinders.edu.au

Adrian D. Werner: adrian.werner@flinders.edu.au

Conflict of interest: None.

Keywords: Groundwater modelling; Boundary conditions; Robin; Cauchy; Mixed.

1 To solve the partial differential equations of groundwater flow, the information about head
2 (h) and/or head gradient (∇h) must be specified along the boundaries of a model domain. The
3 descriptors of different boundary condition (BC) types are drawn from founding
4 mathematicians mainly of the 19th century (Cheng and Cheng 2005). Mathematically, there
5 are five different BC types, including: Dirichlet (Type 1), Neumann (Type 2), Robin (Type
6 3), Cauchy and Mixed (Liu 2018). These names are sometimes used in communicating the
7 BCs of groundwater flow models, and therefore, correct association between nomenclature
8 and the mathematical form of BCs is important for properly communicating model
9 characteristics.

10

11 The distinction between different BC types is consistent across mathematical literature (e.g.,
12 Weisstein 2019). However, there appears to be inconsistencies in the naming of BCs of
13 groundwater flow models, as we demonstrate later in this article. To address this issue, we
14 firstly provide BC definitions in general mathematical forms, as given below. General BC
15 formulae are then translated into standard groundwater flow BCs through, for example,
16 application of Darcy's Law and using conceptualizations commonly adopted in defining BCs
17 for groundwater problems.

18

19 *Dirichlet (Type 1) BC:*

20 The Dirichlet BC derives from the Dirichlet problem, which refers to a boundary problem of
21 closed region Ω , with boundary Γ , where the BC is defined by (Cheng and Cheng 2005):

22
$$\phi = f(\mathbf{x}); \quad \mathbf{x} \in \Gamma \tag{1}$$

23 Here, ϕ is the dependent variable, $f(\mathbf{x})$ is specified as a continuous function, and \mathbf{x} represents
24 temporal and spatial dimensions.

25

26 In groundwater applications of the Dirichlet BC, the hydraulic head (or in some cases the
 27 pressure head), h [L], is specified. The term “specified-head condition” is used where h is
 28 described as a function of space and/or time, whereas h values that are constant (or piecewise
 29 constant) in time and space are referred to as “constant-head conditions” (Franke et al. 1987).
 30 Thus, the Dirichlet BC applied to groundwater flow problems can be written as.

$$31 \quad h = \begin{cases} h_0 & \text{Constant-head boundary} \\ f(\mathbf{x}) & \text{Specified-head boundary} \end{cases} \quad (2)$$

32 where h_0 is a constant.

33

34 Dirichlet BCs most commonly represent the influence of surface water bodies within
 35 groundwater models, for situations where the head imposed on the groundwater system can
 36 be assumed independent of subsurface flow variations. This requires strong groundwater-
 37 surface water connectivity and sufficiently large surface water volumes and/or flow rates that
 38 are stable despite groundwater fluctuations (Bear 1979). Another common application of the
 39 Dirichlet BC to groundwater flow problems is the imposition of atmospheric pressure in
 40 locations of groundwater discharge to the land surface (e.g., a seepage face; Scudeler et al.
 41 2017). This presumes that water does not accumulate to significant depths in surface
 42 depressions and that seepage is continuous and occurs at known locations.

43

44 Neumann (Type 2) BC:

45 In the Neumann BC, the normal derivative of the dependent variable is defined at the
 46 boundary, as (Cheng and Cheng 2005):

$$47 \quad \frac{\partial \phi}{\partial n} = f(\mathbf{x}); \quad \mathbf{x} \in \Gamma \quad (3)$$

48 where n is the outward normal of Γ , and $f(\mathbf{x})$ is a continuous function. For groundwater flow
 49 problems, the normal derivative in the Neumann BC is $\partial h/\partial n$, which implies a specific

50 discharge (or Darcy velocity, q [L/T]) of water into or out of the boundary on the basis of
51 Darcy's Law (Franke et al. 1987). Following the terminology used to define different types of
52 Dirichlet BC, a "specified-flux condition" refers to boundary fluxes that vary in space and/or
53 time, while a "constant-flux condition" refers to boundary fluxes that are constant (or
54 piecewise constant) in time and space (i.e., $\partial h/\partial n = \text{constant}$). Setting $q = 0$ along a
55 groundwater model boundary is a special case, referred to as a "no-flow condition". It is
56 noteworthy that the modeller often sets the volumetric flux normal to the boundary (Q [L³/T])
57 in practical applications of specified- and constant-flux conditions. For confined aquifers,
58 setting Q as constant implies that $\partial h/\partial n$ is constant. However, in situations where the
59 boundary conductance varies (e.g., in models of unconfined aquifers), the ratio between Q
60 and $\partial h/\partial n$ is not constant, and rather, $h\partial h/\partial n$ is constant. Thus, setting Q to a constant value
61 may not lead to a Neumann BC.

62

63 The assignment of no-flow conditions in groundwater models to represent low-permeability
64 strata, geological discontinuities and hydraulic divides is commonplace. Estimates of base
65 flow to rivers and lakes, submarine groundwater discharge to the sea, and recharge through
66 the land surface are routinely used in setting specified- and constant-flux conditions. In
67 practice however, it is less common to know accurately the fluxes into/out of a groundwater
68 system compared to the knowledge of heads, which can be ascertained directly from
69 monitoring wells, and in some cases, surface water levels and topography (e.g., Knowling
70 and Werner 2016).

71

72 *Robin (Type 3) BC:*

73 The Robin BC is a linear combination of the Dirichlet and Neumann BCs, as (Gustafson
74 1999):

75
$$\frac{\partial \phi}{\partial n} + a\phi = f(\mathbf{x}); \quad \mathbf{x} \in \Gamma \quad (4)$$

76 where a [L^{-1}] is a non-zero coefficient, which might be constant or variable. Replacing ϕ with
 77 h , applying Darcy's Law, and setting a to $-1/L$ and $f(\mathbf{x})$ to $-h_{\text{ref}}/L$, the follow formula is
 78 obtained that is readily applicable to flow across a model boundary:

79
$$Q = -\frac{KA}{L}(h - h_{\text{ref}}) \quad (5)$$

80 where K [L/T] is aquifer hydraulic conductivity, A is the cross-sectional area of the boundary
 81 through which groundwater flows, h_{ref} is a reference head representing an externality to the
 82 model domain, and L is the length over which the head drop $h - h_{\text{ref}}$ occurs. The common
 83 name in hydrogeological literature for BCs of the form given in equation (5) is “head-
 84 dependent flux condition” (e.g., Harbaugh 2005). This description refers to the reliance of Q
 85 on h at the boundary. It is commonplace to refer to KA/L as the “boundary conductance”, C
 86 [L^2/T]. Both C and h_{ref} may vary in space and time.

87

88 The Robin BC can be applied in groundwater modelling to represent the truncation of
 89 aquifers, whereby regions of aquifer that fall outside of the model domain are approximated
 90 by C and h_{ref} . Additionally, flow to/from a river (in situations where the groundwater level is
 91 higher than the river bed) is often represented using equation (5), with impedance to flow
 92 caused by the river bed included in the parameterization of C (e.g., Werner and Laattoe
 93 2016).

94

95 As mentioned above, setting Q to a constant value for an unconfined aquifer situation implies
 96 that $h\partial h/\partial n$ is constant. This can be written as $\partial h/\partial n - a/h = 0$, and therefore, $\partial h/\partial n$ and h are
 97 inversely related. Strictly speaking, this falls outside of BC forms that are defined in the
 98 current article.

99

100 Cauchy BC:

101 In the Cauchy BC, both the dependant variable and its normal derivative must be specified
102 along the boundary. This corresponds to the imposition of both Dirichlet and Neumann BCs
103 (Arfken and Weber 2005; Liu 2018). The Cauchy BC can be expressed as:

$$104 \quad \begin{cases} \phi = f(\mathbf{x}); \\ \frac{\partial \phi}{dn} = g(\mathbf{x}); \end{cases} \quad \mathbf{x} \in \Gamma \quad (6)$$

105 where, $g(\mathbf{x})$ is a continuous function.

106

107 Application of equation (6) to groundwater models implies knowledge of both q (via Darcy's
108 Law) and h at the boundary. Practical groundwater problems for which both q and h are
109 known are rare, to the degree that we were unable to find examples where equation (6) has
110 been applied to a real-world groundwater modelling case.

111

112 Mixed BC:

113 The Mixed BC refers to the case in which the boundary consists of non-overlapping
114 segments, each having different BC types (Griffiths et al. 2015). For example, if the boundary
115 (Γ) consists of two disjoint parts: Γ_D with a Dirichlet BC and Γ_N with a Neumann BC, this is
116 considered as a Mixed BC, given by (Cheng and Cheng 2005; Liu 2018):

$$117 \quad \begin{cases} \phi = f(\mathbf{x}); & \mathbf{x} \in \Gamma_D \\ \frac{\partial \phi}{dn} = g(\mathbf{x}); & \mathbf{x} \in \Gamma_N \end{cases} \quad \text{where } \Gamma_D \cup \Gamma_N = \Gamma \quad (7)$$

118

119 The vast majority of groundwater models applied to practical situations comprise multiple
120 BC types, because various combinations of recharge, pumping, surface water controls,

121 geological boundaries, groundwater divides (i.e., lines connecting high points in a
122 potentiometric surface thereby acting as a no-flow boundary from which water flows in
123 opposite directions), streamlines (i.e., advective pathways of water particles) and
124 evapotranspiration (e.g., in 2D vertical cross-section models) are used to define external
125 stresses acting on model domain. Therefore, using the standard definition given above, it
126 could be said that almost all practical groundwater models have Mixed BCs, which thus does
127 not differentiate in a meaningful way one groundwater model from another.

128

129 **Inconsistencies in BC definitions**

130

131 Mathematical literature is consistent in describing equation (4) as the Robin BC, which is
132 also referred to as a Type 3 (or “third-type”) BC (e.g., Gustafson and Abe 1998). Equation
133 (5), obtained by substitution of groundwater parameters into equation (4), defines a
134 relationship where Q is dependent on h , and therefore the term “head-dependent flux” is a
135 logical description of the Robin BC in groundwater applications. A review of prominent
136 groundwater references finds, however, significant inconsistencies in the description of BCs
137 that adopt equation (4), or that refer to “Robin BC”, “type 3” (or “third type”) or “head-
138 dependent flux” conditions, as summarized in Table 1.

139

140 **Table 1.** Terminology used in describing BCs in the form of equation (4) (i.e., Robin BC).

Reference	Referenced description of Robin BC
Bear (1972), p252	“third, or Cauchy boundary value problem”
Bear (1979), p98, 220	“mixed boundary condition (boundary condition of third type; Cauchy boundary condition)”
Bear and Verruijt (1987), p72, 152	“mixed boundary condition, boundary condition of the third kind, or a Cauchy condition”
Franke et al. (1987), p6	“head-dependent flux, Type 3 (mixed boundary condition), Cauchy”
Guo and Langevin (2002), p15, 16, 17	“Cauchy (head-dependent flux or mixed boundary condition; Type III)”
COMSOL (2005), p16, 18, 19, 24, 89, 90, 105	“Mixed, Cauchy condition”
Holzbecher (2007), p62, 81	“3 rd type, Cauchy - or Robin boundary condition”
Bear and Cheng (2010), p189, 198, 313, 439	“boundary condition of the third type, or a Robin boundary condition”
Barnett et al. (2012), p54, 169	“Type 3, Cauchy or specified head and gradient boundary condition; Type 3 (Cauchy, or mixed)”
Diersch (2014), p196	“Cauchy-Type (3rd Kind) BC”
Anderson et al. (2015), p77	“Type 3. Head-dependent boundary (Cauchy condition)”
Thangarajan and Singh (2016), p239	“Mixed type boundary condition or Cauchy-type boundary condition or head dependent flow boundary; Robin type boundary condition”
De Smedt and Zijl (2017), p21	“third-type boundary condition (Robin boundary condition)”
DHI (2017)	“Cauchy-type BCs; Fluid-transfer BCs; ‘general head’ boundaries”
USGS (2018)	“Head-Dependent Flux (Robin or mixed boundary condition)”

141
142 Inconsistencies in the description of the Robin BC include prominent references widely used
143 by the groundwater community. For example, Bear (1972; 1979) and Bear and Verruijt
144 (1987) refer to Robin BCs as “Cauchy” and “Mixed” BCs, although Bear and Cheng (2010)
145 correctly define BCs in the form of equation (4) as the Robin BC. Bear (1972; 1979), Bear
146 and Verruijt (1987) and Bear and Cheng (2010) consistently refer to the same form of BC
147 equation as “third” type. The Australian Groundwater Modelling Guideline (Barnett 2012)
148 refers to “head-dependent BC” as “Type 3”, but labels these as “Cauchy”, rather than
149 “Robin” BCs. User manuals for widely used groundwater models (e.g., Guo and Langevin
150 2002; COMSOL 2005; DHI 2017) refer to the Robin BC as “Cauchy” (and sometimes
151 “Mixed”), whereas USGS (2018) correctly identify the Robin BC, although they consider it

152 also to be a “Mixed” BC. Of the references in Table 1, only Bear and Cheng (2010) and de
 153 Smedt and Zijl (2017) correctly describe the Robin BC.

154

155 Given MODFLOW’s widespread use, packages commonly applied to represent BCs should
 156 be correctly labelled according to the previous BC definitions. In attempting to do this, we
 157 find that there are BCs that switch between different BC types, usually Neumann and Robin
 158 BCs. This is demonstrated in Table 2, which outlines the mathematical constructs of several
 159 popular packages.

160

161 **Table 2.** MODFLOW packages defined according to standard BC types.

Application	Mathematical representation (Harbaugh 2005)	Type of BC
GHB package (general-head boundary)	$q = C(h_{\text{ref}} - h)$ h_{ref} : external source head	Robin
RIV package (river)	$q = \begin{cases} C(h_{\text{ref}} - h) & h > h_{\text{bot}} \\ C(h_{\text{ref}} - h_{\text{bot}}) & h \leq h_{\text{bot}} \end{cases}$ h_{ref} : river water level (stage) h_{bot} : river bottom bed elevation	Robin Neumann
DRN package (drain)	$q = \begin{cases} C(h - h_{\text{ref}}) & h > h_{\text{ref}} \\ 0 & h \leq h_{\text{ref}} \end{cases}$ h_{ref} : drain bed elevation	Robin Neumann
EVT package (evapotranspiration)	$q = \begin{cases} q_{\text{max}} & h > h_{\text{sur}} \\ q_{\text{max}} \frac{h - (h_{\text{sur}} - h_{\text{ext}})}{h_{\text{ext}}} & (h_{\text{sur}} - h_{\text{ext}}) \leq h \leq h_{\text{sur}} \\ 0 & h < (h_{\text{sur}} - h_{\text{ext}}) \end{cases}$ q_{max} : maximum possible value of q h_{sur} : surface elevation h_{ext} : extinction depth	Neumann Robin Neumann

162

163 The switching of BC types relying on the dependent variable (h) has not been labelled in
 164 previous mathematical literature, although BCs of this type are sometimes referred to as
 165 “Mixed BCs” (see Table 1). Therefore, we recommend the term “switching condition”,
 166 followed by an explanation of the BC types that switch within this condition (in the case of
 167 Table 2, the Robin and Neumann BC types). Another example of a switching BC (using the

168 definition herein) is described by Shoushtari et al. (2015), whereby the seepage face exit
169 point shifts along the beach slope under tidal forcing, causing switching between Dirichlet
170 and Neumann BC types.

171

172 It is clear from our review of the groundwater literature that correction and revision to the
173 descriptions of groundwater flow BCs are needed, even though errors in mathematical
174 definitions of BCs were not encountered per se. Most groundwater references appear to
175 misname the Robin BC as “Cauchy” and/or “Mixed”. In Barnett et al. (2012), the Cauchy BC
176 is correctly defined for solute transport, but then “Cauchy” is adopted for head-dependent
177 flow BCs, for which Robin BC is the correct description. While we have not considered the
178 nomenclature of solute transport BCs in groundwater literature, a review of these is likely
179 warranted given the issues with groundwater flow BC descriptions.

180

181 **Acknowledgements**

182

183 The authors appreciate the suggestions of Eve Kuniandy and one anonymous reviewer that
184 led to improvements of the manuscript. Adrian Werner is the recipient of an Australian
185 Research Council Future Fellowship (project number FT150100403). Amir Jazayeri is
186 funded by the Australian Research Council (project numbers FT150100403 and
187 LP140100317).

188

189 **References**

190

191 Anderson, M.P., W.W. Woessner, and R.J. Hunt. 2015. *Applied Groundwater Modeling:
192 Simulation of Flow and Advective Transport*. Amsterdam: Elsevier Academic Press.

193

194 Arfken, G.B., and H.J. Weber. 2005. *Mathematical Methods for Physicists*. Amsterdam:
195 Elsevier Academic Press.

196

197 Barnett, B., L. Townley, V. Post, R.E. Evans, R.J. Hunt, L. Peeters, S. Richardson, A.D.
198 Werner, A. Knapton, and A. Boronkay. 2012. *Australian groundwater modelling guidelines*.
199 Sinclair Knight Merz and National Centre for Groundwater Research and Training.
200 Waterlines Report Series No. 82. Canberra: National Water commission.

201

202 Bear, J. 1972. *Dynamics of Fluids in Porous Media*. New York: American Elsevier
203 Publishing Company Inc.

204

205 Bear, J. 1979. *Hydraulics of Groundwater*. New York: McGraw-Hill.

206

207 Bear, J., and A. Verruijt. 1987. *Modeling Groundwater Flow and Pollution: With Computer*
208 *Programs for Sample Cases*. Dordrecht: D. Reidel Publishing Co.

209

210 Bear, J., and A.H.-D. Cheng. 2010. *Modeling Groundwater Flow and Contaminant*
211 *Transport*. Dordrecht: Springer.

212

213 Cheng, A.H.-D., and D.T. Cheng. 2005. Heritage and early history of the boundary element
214 method. *Engineering Analysis with Boundary Elements* 29: 268–302. DOI:
215 10.1016/j.enganabound.2004.12.001.

216

217 COMSOL. 2005. *Earth Science Module User's Guide: Version 3.2*. Stockholm: COMSOL
218 AB.

219

220 De Smedt, F., and W. Zijl. 2017. *Two- and Three-Dimensional Flow of Groundwater*. Boca
221 Raton: CRC Press.

222

223 Diersch, H.-J.G. 2014. *FEFLOW: Finite Element Modeling of Flow, Mass and Heat*
224 *Transport in Porous and Fractured Media*. Berlin: Springer.

225

226 Franke, O.L., T.E. Reilly, and G.D. Bennett. 1987. *Definition of Boundary and Initial*
227 *Conditions in the Analysis of Saturated Ground-Water Flow Systems: An Introduction*.
228 Techniques of Water-Resources Investigations of the U.S. Geological Survey. Book 3, Chap.
229 B5. Washington: USGS.

230

231 DHI. 2017. FEFLOW 7.1 Documentation.
232 http://www.feflow.info/html/help71/feflow/mainpage.htm#t=09_Parameters%2FBoundary_C
233 [onditions%2Fboundaryconditions.html%3Frhlterm%3Dcauchy%26rhsyns%3D%2520](http://www.feflow.info/html/help71/feflow/mainpage.htm#t=09_Parameters%2FBoundary_C)
234 (accessed February 22, 2019).

235

236 Griffiths, D.F., J.W. Dold, and D.J. Silvester. 2015. *Essential Partial Differential Equations:*
237 *Analytical and Computational Aspects*. Cham: Springer.

238

239 Guo, W., and C.D. Langevin. 2002. *User's Guide to SEAWAT: A Computer Program For*
240 *Simulation of Three-Dimensional Variable-Density Ground-Water Flow*. Techniques of
241 Water-Resources Investigations of the U.S. Geological Survey. Book 6, Chap. A7.
242 Tallahassee: USGS.

243

244 Gustafson, K.E. 1999. *Introduction to Partial Differential Equations and Hilbert Space*
245 *Methods*. New York: Dover Publications, Inc.
246
247 Gustafson, K., and T. Abe. 1998. The third boundary condition—was it Robin's? *The*
248 *Mathematical Intelligencer* 20: 63–71. DOI: 10.1007/BF03024402.
249
250 Harbaugh, A.W. 2005. *MODFLOW-2005, The U.S. Geological Survey Modular Ground-*
251 *Water Model—the Ground-Water Flow Process*. U.S. Geological Survey Techniques and
252 Methods. Book 6, Chap. A16. Reston: USGS.
253
254 Holzbecher, E. 2007. *Environmental Modeling Using MATLAB*. Berlin: Springer.
255
256 Knowling, M.J., and A.D. Werner. 2016. Estimability of recharge through groundwater
257 model calibration: insights from a field-scale steady-state example. *Journal of Hydrology*
258 540: 973–987. DOI: 10.1016/j.jhydrol.2016.07.003.
259
260 Liu, Z.L. 2018. *Multiphysics in Porous Materials*. Cham: Springer. DOI: 10.1007/978-3-319-
261 93028-2.
262
263 Shoushtari S.M.H., P. Nielsen, N. Cartwright, and P. Perrochet. 2015. Periodic seepage face
264 formation and water pressure distribution along a vertical boundary of an aquifer. *Journal of*
265 *Hydrology* 523: 24–33. DOI: 10.1016/j.jhydrol.2015.01.027.
266
267 Scudeler, C., C. Paniconi, D. Pasetto, and M. Putti. 2017. Examination of the seepage face
268 boundary condition in subsurface and coupled surface/subsurface hydrological models, *Water*
269 *Resources Research* 53, no. 3: 1799–1819. DOI: 10.1002/2016WR019277.

270

271 Thangarajan, M., and V.P. Singh. 2016. *Groundwater Assessment, Modeling, and*
272 *Management*. Boca Raton: CRC Press.

273

274 USGS. 2018. Online Guide to MODFLOW-2005.

275 <https://water.usgs.gov/ogw/modflow/MODFLOW-2005-Guide/index.html?bcf.htm> (accessed
276 February 22, 2019).

277

278 Weisstein, E.W. 2019. Boundary Conditions, MathWorld - A Wolfram Web Resource.

279 <http://mathworld.wolfram.com/BoundaryConditions.html> (accessed February 22, 2019).

280

281 Werner, A.D., and T. Laattoe. 2016. Terrestrial freshwater lenses in stable riverine settings:

282 Occurrence and controlling factors. *Water Resources Research* 52, no. 5: 3654–3662.

283 DOI:10.1002/2015WR018346.

284